

## 11.F.1. Derivation of the Hydrodynamic Equations

The **particle density** is defined as

$$\begin{aligned}
 n(\mathbf{r}, t) &= n_N(\mathbf{r}, t) + n_M(\mathbf{r}, t) \\
 &= \int d\mathbf{p} \left[ f_N(\mathbf{r}, \mathbf{p}, t) + f_M(\mathbf{r}, \mathbf{p}, t) \right] \\
 &= \int d\mathbf{p} f^0(\mathbf{p}) \left[ 2 + h^+(\mathbf{r}, \mathbf{p}, t) \right] && [ (11.88-9) \text{ used. } ] && (11.128) \\
 &= \frac{n_0}{2} \langle 1, 2 + h^+ \rangle && [ n_0 = \frac{N}{V} ] \\
 &= n_0 + \frac{n_0}{2} \langle 1, h^+ \rangle
 \end{aligned}$$

Using  $\hat{C}^+ 1 = 0$ , the Boltzmann equation (11.96) in the absence of external forces (i.e.,  $\dot{\mathbf{p}} = 0$ ),

$$\frac{\partial h^+}{\partial t} + \frac{\mathbf{p}}{m} \cdot \frac{\partial h^+}{\partial \mathbf{r}} = \hat{C}^+ h^+ \quad (11.128a)$$

can be written as

$$\frac{\partial (2 + h^+)}{\partial t} + \frac{\mathbf{p}}{m} \cdot \frac{\partial (2 + h^+)}{\partial \mathbf{r}} = \hat{C}^+ (2 + h^+) \quad (11.128b)$$

$\frac{n_0}{2} \langle 1, (11.128b) \rangle$  gives

$$\begin{aligned}
 \frac{\partial n}{\partial t} + \int d\mathbf{p} f^0 \frac{\mathbf{p}}{m} \cdot \frac{\partial h^+}{\partial \mathbf{r}} &= \frac{n_0}{2} \langle 1, \hat{C}^+ (2 + h^+) \rangle \\
 &= \frac{n_0}{2} \langle \hat{C}^+ 1, 2 + h^+ \rangle = 0
 \end{aligned} \quad (11.128c)$$

The **particle flux ( current density )** is defined as

$$\begin{aligned}
 \mathbf{J}^n(\mathbf{r}, t) &= \int d\mathbf{p} \frac{\mathbf{p}}{m} \left[ f_N(\mathbf{r}, \mathbf{p}, t) + f_M(\mathbf{r}, \mathbf{p}, t) \right] \\
 &= \int d\mathbf{p} \frac{\mathbf{p}}{m} f^0(\mathbf{p}) \left[ 2 + h^+(\mathbf{r}, \mathbf{p}, t) \right] \\
 &= \int d\mathbf{p} \frac{\mathbf{p}}{m} f^0(\mathbf{p}) h^+(\mathbf{r}, \mathbf{p}, t)
 \end{aligned} \quad (11.130)$$

where we have used

$$\begin{aligned}
 \int d\mathbf{p} \frac{\mathbf{p}}{m} f^0(\mathbf{p}) &= - \int d\mathbf{p} \frac{\mathbf{p}}{m} f^0(\mathbf{p}) && [ \mathbf{p} \rightarrow -\mathbf{p} ] \\
 &= 0 && [ a = -a \rightarrow a = 0 ]
 \end{aligned}$$

Since  $\mathbf{r}$  &  $\mathbf{p}$  are independent variables,

$$\nabla_r \cdot \mathbf{J}^n(\mathbf{r}, t) = \int d\mathbf{p} f^0 \frac{\mathbf{p}}{m} \cdot \frac{\partial h^+}{\partial \mathbf{r}}$$

so that (11.128c) becomes

$$\frac{\partial n}{\partial t} + \nabla_r \cdot \mathbf{J}^n = 0 \quad (11.129)$$

which can be identified as the **mass balance equation** [ c.f. (10.3) of §10.B.1.1 with  $\rho = mn$  ].

The **velocity field** is defined as

$$\mathbf{v}(\mathbf{r}, t) = \frac{\mathbf{J}^n(\mathbf{r}, t)}{n(\mathbf{r}, t)}$$

which, to 1st order in  $h^+$ , becomes

$$\mathbf{v}(\mathbf{r}, t) = \frac{\mathbf{J}^n(\mathbf{r}, t)}{n_0}$$

(11.129) then simplifies to

$$\frac{\partial n}{\partial t} + n_0 \nabla_r \cdot \mathbf{v} = 0 \quad (11.131)$$

which is the **linearized continuity equation** that describes the conservation of the total number of particles.

For the reverse scattering,

$$t \rightarrow -t \Rightarrow \quad \mathbf{p} \rightarrow -\mathbf{p}$$

(11.94) then gives

$$h^+ \rightarrow h^+$$

so that (11.130) gives

$$\mathbf{J}^n \rightarrow -\mathbf{J}^n \quad \rightarrow \quad \mathbf{v} \rightarrow -\mathbf{v}$$

(11.131) is therefore invariant under time reversal, i.e., it contains no irreversible effects. Irreversible phenomena, such as decay to equilibrium, must come from the other hydrodynamic equations.

Using

$$\begin{aligned} \hat{\mathbf{C}}^+ \mathbf{p} &= 2 \int d\mathbf{p}' \int d\Omega \, v \sigma(b, v) f^{0'}(\mathbf{p}_f - \mathbf{p} + \mathbf{p}_f' - \mathbf{p}') \\ &= 0 \quad \text{[ Momentum conservation used. ]} \end{aligned}$$

$\frac{n_0}{2m} \langle \mathbf{p}, (11.128 a) \rangle$  gives

$$\begin{aligned} \frac{\partial \mathbf{J}^n}{\partial t} + \int d\mathbf{p} \frac{\mathbf{p}}{m} f^0(\mathbf{p}) \frac{p_j}{m} \frac{\partial h^+}{\partial r_j} &= \frac{n_0}{2m} \langle \mathbf{p}, \hat{\mathbf{C}}^+ h^+ \rangle \\ &= \frac{n_0}{2m} \langle \hat{\mathbf{C}}^+ \mathbf{p}, h^+ \rangle = 0 \end{aligned} \quad (11.132a)$$

Defining the **pressure tensor** as

$$\mathbb{P}_{ij}(\mathbf{r}, t) = \frac{1}{m} \int d\mathbf{p} f^0(\mathbf{p}) p_i p_j h^+(\mathbf{r}, \mathbf{p}, t) = \mathbb{P}_{ji} \quad (11.133)$$

we have

$$\nabla_r \cdot \mathbb{P} = \frac{1}{m} \int d\mathbf{p} f^0(\mathbf{p}) p_i \frac{\partial h^+}{\partial r_i} \mathbf{p}$$

so that (11.132a) becomes

$$m \frac{\partial \mathbf{J}^n}{\partial t} + \nabla_r \cdot \mathbb{P} = 0 \quad (11.132)$$

which can be identified as the **momentum balance equation** in the absence of external forces. Comparing with (10.8) of §10.B.1.2, we have

$$\mathbb{P} = P \mathbb{I} + \rho \mathbf{v} \mathbf{v} + \mathbb{\Pi} \quad [\rho = m n] \quad (11.132a)$$

where the convective term  $\rho \mathbf{v} \mathbf{v}$  will be neglected in the linearized equation and the **stress tensor**  $\mathbb{\Pi}$  contains (irreversible) viscous effects caused by collisions.

Since the particles are free except for brief moments of collisions, the **total average energy density** is

$$\epsilon(\mathbf{r}, t) = \int d\mathbf{p} \frac{\mathbf{p}^2}{2m} \left[ f_N(\mathbf{r}, \mathbf{p}, t) + f_M(\mathbf{r}, \mathbf{p}, t) \right]$$

$$\begin{aligned}
&= \int d\mathbf{p} \frac{\mathbf{p}^2}{2m} f^0(\mathbf{p}) \left[ 2 + h^+(r, \mathbf{p}, t) \right] \\
&= \frac{n_0}{2} \left\langle \frac{\mathbf{p}^2}{2m}, 2 + h^+ \right\rangle \\
&= n_0 \left( \frac{\beta}{2\pi m} \right)^{3/2} \int d\mathbf{p} \frac{\mathbf{p}^2}{2m} e^{-\beta p^2/2m} + \int d\mathbf{p} \frac{\mathbf{p}^2}{2m} f^0(\mathbf{p}) h^+(r, \mathbf{p}, t) \\
&= \kappa + u(r, t)
\end{aligned} \tag{11.135a}$$

where, for our ideal-gas-like system,

$$\kappa = n_0 \left( \frac{\beta}{2\pi m} \right)^{3/2} \int d\mathbf{p} \frac{\mathbf{p}^2}{2m} e^{-\beta p^2/2m} \tag{11.135b}$$

can be taken as its **kinetic energy density** and

$$u(r, t) = \int d\mathbf{p} \frac{\mathbf{p}^2}{2m} f^0(\mathbf{p}) h^+(r, \mathbf{p}, t) = \frac{n_0}{2} \left\langle \frac{\mathbf{p}^2}{2m}, h^+ \right\rangle \tag{11.135}$$

its **internal energy density**.

Thus,  $\frac{n_0}{2} \left\langle \frac{\mathbf{p}^2}{2m}, (11.128 b) \right\rangle$  gives

$$\begin{aligned}
\frac{\partial \epsilon}{\partial t} + \int d\mathbf{p} f^0 \frac{\mathbf{p}^2}{2m} \frac{\mathbf{p}}{m} \cdot \frac{\partial h^+}{\partial \mathbf{r}} &= \frac{n_0}{2} \left\langle \frac{\mathbf{p}^2}{2m}, \hat{C}^+(2 + h^+) \right\rangle \\
&= \frac{n_0}{4m} \left\langle \hat{C}^+ \mathbf{p}^2, 2 + h^+ \right\rangle = 0
\end{aligned} \tag{11.134a}$$

where  $\hat{C}^+ \mathbf{p}^2 = 0$  owing to energy conservation [see 3rd solution to (11.101b) in §11.D.2].

The **energy flux (current density)** is defined as

$$\begin{aligned}
\mathbf{J}^\epsilon(r, t) &= \int d\mathbf{p} \frac{\mathbf{p}^2}{2m} \frac{\mathbf{p}}{m} f^0(\mathbf{p}) \left[ f_N(r, \mathbf{p}, t) + f_M(r, \mathbf{p}, t) \right] \\
&= \int d\mathbf{p} \frac{\mathbf{p}^2}{2m} \frac{\mathbf{p}}{m} f^0(\mathbf{p}) \left[ 2 + h^+(r, \mathbf{p}, t) \right] \\
&= \int d\mathbf{p} \frac{\mathbf{p}^2}{2m} \frac{\mathbf{p}}{m} f^0(\mathbf{p}) h^+(r, \mathbf{p}, t)
\end{aligned} \tag{11.136}$$

where we have used

$$\begin{aligned}
\int d\mathbf{p} \frac{\mathbf{p}^2}{2m} \frac{\mathbf{p}}{m} f^0(\mathbf{p}) &= - \int d\mathbf{p} \frac{\mathbf{p}^2}{2m} \frac{\mathbf{p}}{m} f^0(\mathbf{p}) && [\mathbf{p} \rightarrow -\mathbf{p}] \\
&= 0 && [a = -a \rightarrow a = 0]
\end{aligned}$$

Since  $\mathbf{r}$  &  $\mathbf{p}$  are independent variables,

$$\nabla_r \cdot \mathbf{J}^\epsilon(r, t) = \int d\mathbf{p} f^0 \frac{\mathbf{p}^2}{2m} \frac{\mathbf{p}}{m} \cdot \frac{\partial h^+}{\partial \mathbf{r}}$$

so that (11.134a) becomes

$$\frac{\partial \epsilon}{\partial t} + \nabla_r \cdot \mathbf{J}^\epsilon = 0 \tag{11.134}$$

which can be identified as the **energy balance equation**.

The **average energy per particle**  $e(r, t)$  is defined by

$$\epsilon(r, t) = n(r, t) e(r, t) \tag{11.134a}$$

$$\begin{aligned} \rightarrow \quad \frac{\partial \epsilon}{\partial t} &= \frac{\partial n}{\partial t} e + n \frac{\partial e}{\partial t} \\ &\approx \frac{\partial n}{\partial t} e_0 + n_0 \frac{\partial e}{\partial t} \end{aligned} \quad \text{[ Linearized. ]} \quad (11.137a)$$

where

$$e_0 = \frac{\kappa}{n_0} = \left( \frac{\beta}{2\pi m} \right)^{3/2} \int d\mathbf{p} \frac{\mathbf{p}^2}{2m} e^{-\beta \mathbf{p}^2/2m}$$

is the average (kinetic) energy of a free particle.

(11.134) thus becomes

$$n_0 \frac{\partial e}{\partial t} + e_0 \frac{\partial n}{\partial t} + \nabla_r \cdot \mathbf{J}^\epsilon = 0 \quad (11.137)$$

As in §10.B.3, we decompose the stress tensor  $\Pi$  as

$$\Pi = -\zeta \nabla_r \cdot \mathbf{v} - 2\eta [\nabla_r \mathbf{v}]^s \quad \text{[ (10.30-1) used. ]}$$

$$\rightarrow \quad \Pi_{ij} = -\delta_{ij} \zeta \nabla_r \cdot \mathbf{v} - \eta \left( \frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \nabla_r \cdot \mathbf{v} \right) \quad \text{[ See Ex.10.2 of §10.B.3. ]}$$

The pressure tensor (11.132a) thus becomes

$$\begin{aligned} \mathbf{P}_{ij} &= P \delta_{ij} + m n v_i v_j - \delta_{ij} \zeta \nabla_r \cdot \mathbf{v} - \eta \left( \frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \nabla_r \cdot \mathbf{v} \right) \\ &\approx P \delta_{ij} - \delta_{ij} \zeta \nabla_r \cdot \mathbf{v} - \eta \left( \frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \nabla_r \cdot \mathbf{v} \right) \end{aligned} \quad \text{[ Linearized. ]} \quad (11.138)$$

$$\begin{aligned} \rightarrow \quad \nabla_r \cdot \mathbf{P} &= \partial_j \mathbf{P}_{ij} \\ &\approx \partial_j P - \zeta \partial_j \nabla_r \cdot \mathbf{v} - \eta \left( \frac{\partial \nabla_r \cdot \mathbf{v}}{\partial x_j} + \nabla_r^2 v_j - \frac{2}{3} \partial_j \nabla_r \cdot \mathbf{v} \right) \\ &= \nabla_r P - \zeta \nabla_r (\nabla_r \cdot \mathbf{v}) - \eta \left( \nabla_r (\nabla_r \cdot \mathbf{v}) + \nabla_r^2 \mathbf{v} - \frac{2}{3} \nabla_r (\nabla_r \cdot \mathbf{v}) \right) \\ &= \nabla_r P - \left( \zeta + \frac{1}{3} \eta \right) \nabla_r (\nabla_r \cdot \mathbf{v}) - \eta \nabla_r^2 \mathbf{v} \end{aligned} \quad (11.138a)$$

Putting (11.138a) into (11.132) gives the linearized momentum balance equation

$$m n_0 \frac{\partial \mathbf{v}}{\partial t} = -\nabla_r P + \left( \zeta + \frac{1}{3} \eta \right) \nabla_r (\nabla_r \cdot \mathbf{v}) + \eta \nabla_r^2 \mathbf{v} \quad (11.139)$$

Under time reversal,

$$\begin{aligned} t \rightarrow -t \quad \mathbf{v}(\mathbf{r}, -t) &= -\mathbf{v}(\mathbf{r}, t) & P(\mathbf{r}, -t) &= P(\mathbf{r}, t) \\ \rightarrow \quad \frac{\partial \mathbf{v}(\mathbf{r}, -t)}{\partial (-t)} &= \frac{\partial \mathbf{v}(\mathbf{r}, t)}{\partial t} & \nabla_r P(\mathbf{r}, -t) &= \nabla_r P(\mathbf{r}, t) \end{aligned}$$

Hence,  $\nabla_r P$  is reactive ( invariant under time reversal ) while the rest of the R.H.S. of (11.139) is dissipative ( changes sign under time reversal ).

Combining (11.131) with (11.137) gives

$$n_0 \frac{\partial e}{\partial t} - n_0 e_0 \nabla_r \cdot \mathbf{v} + \nabla_r \cdot \mathbf{J}^\epsilon = 0 \quad (11.139a)$$

On the other hand, from the 1st law

$$dU = T dS - P dV$$

we have

$$du = T ds + \frac{P}{n^2} dn$$

where

$$u = \frac{U}{N} \quad s = \frac{S}{N} \quad n = \frac{N}{V}$$

Hence,

$$\frac{\partial e}{\partial t} = \frac{\partial u}{\partial t} = T \frac{\partial s}{\partial t} + \frac{P}{n^2} \frac{\partial n}{\partial t} \quad [ \text{ See (11.135a). } ]$$

$$\approx T_0 \frac{\partial s}{\partial t} - \frac{P_0}{n_0} \nabla_r \cdot \mathbf{v} \quad [ (11.131) \text{ used \& linearized. } ] \quad (11.139b)$$

where the subscript 0 denotes an equilibrium value.

Putting the linearized entropy balance equation [ see (10.38) of §10.C.1 ]

$$m n_0 \frac{\partial s}{\partial t} = \frac{K}{T_0} \nabla_r^2 T \quad (11.143)$$

into (11.139b) gives

$$\frac{\partial e}{\partial t} \approx \frac{K}{n_0} \nabla_r^2 T - \frac{P_0}{n_0} \nabla_r \cdot \mathbf{v} \quad (11.143a)$$

Comparing with (11.139a) then gives

$$K \nabla_r^2 T - P_0 \nabla_r \cdot \mathbf{v} - n_0 e_0 \nabla_r \cdot \mathbf{v} + \nabla_r \cdot \mathbf{J}^\epsilon = 0$$

$$\rightarrow \mathbf{J}^\epsilon = -K \nabla_r T + P_0 \mathbf{v} + n_0 e_0 \mathbf{v} \quad (11.140)$$

Note that the hydrodynamic equations (11.131, 139 & 143) are exactly the per-particle version of the linearized equations (10.36-8). We have therefore established a link between the macroscopic & microscopic descriptions of transport via the Boltzmann equation.

Choose  $(n, T)$  as the independent thermodynamic variables, we have, for the linearized equations,

$$\nabla_r P = \left( \frac{\partial P}{\partial n} \right)_T \nabla_r n + \left( \frac{\partial P}{\partial T} \right)_n \nabla_r T \quad (11.140a)$$

$$\frac{\partial s}{\partial t} = \left( \frac{\partial s}{\partial n} \right)_T \frac{\partial n}{\partial t} + \left( \frac{\partial s}{\partial T} \right)_n \frac{\partial T}{\partial t} \quad (11.140b)$$

where the superscript 0 denotes equilibrium values.

The linearized hydrodynamic equations then become

$$\frac{\partial n}{\partial t} + n_0 \nabla_r \cdot \mathbf{v} = 0 \quad [ \text{ same as (11.131) } ] \quad (11.144)$$

$$m n_0 \frac{\partial \mathbf{v}}{\partial t} = - \left( \frac{\partial P}{\partial n} \right)_T \nabla_r n - \left( \frac{\partial P}{\partial T} \right)_n \nabla_r T + \eta \nabla_r^2 \mathbf{v} + \left( \zeta + \frac{1}{3} \eta \right) \nabla_r (\nabla_r \cdot \mathbf{v}) \quad (11.145)$$

$$m n_0 \left( \frac{\partial s}{\partial n} \right)_T \frac{\partial n}{\partial t} + m n_0 \left( \frac{\partial s}{\partial T} \right)_n \frac{\partial T}{\partial t} = \frac{K}{T_0} \nabla_r^2 T \quad (11.146)$$

Switching to the normal mode description (or Fourier transforms), we set

$$n(\mathbf{r}, t) = n_{\mathbf{k}}(\omega) e^{i\mathbf{k} \cdot \mathbf{r} - i\omega t} \quad (11.147)$$

$$\mathbf{v}(\mathbf{r}, t) = \mathbf{v}_k(\omega) e^{i\mathbf{k} \cdot \mathbf{r} - i\omega t} \quad (11.148)$$

$$T(\mathbf{r}, t) = T_k(\omega) e^{i\mathbf{k} \cdot \mathbf{r} - i\omega t} \quad (11.149)$$

so that (11.144-6) become

$$-i\omega n_k(\omega) + i n_0 \mathbf{k} \cdot \mathbf{v}_k(\omega) = 0 \quad (11.149a)$$

$$-i\omega m n_0 \mathbf{v}_k(\omega) = -i \left( \frac{\partial P}{\partial n} \right)_T \mathbf{k} n_k(\omega) - i \left( \frac{\partial P}{\partial T} \right)_n \mathbf{k} T_k(\omega) \quad (11.149b)$$

$$-\eta k^2 \mathbf{v}_k(\omega) - \left( \zeta + \frac{1}{3} \eta \right) \mathbf{k} [\mathbf{k} \cdot \mathbf{v}_k(\omega)]$$

$$-i\omega m n_0 \left( \frac{\partial s}{\partial n} \right)_T n_k(\omega) - i\omega m n_0 \left( \frac{\partial s}{\partial T} \right)_n T_k(\omega) = -\frac{K}{T_0} k^2 T_k(\omega) \quad (11.149c)$$

As in §10.C.1, we set [ c.f. (10.50) ]

$$\mathbf{v}_k(\omega) = v_k^{\parallel}(\omega) \hat{\mathbf{k}} + \mathbf{v}_k^{\perp}(\omega) \quad [ \hat{\mathbf{k}} \cdot \mathbf{v}_k^{\perp}(\omega) = 0 ] \quad (11.149a)$$

The transverse modes involve only (11.149b), which gives

$$-i\omega m n_0 \mathbf{v}_k^{\perp}(\omega) = -\eta k^2 \mathbf{v}_k^{\perp}(\omega)$$

$$\rightarrow (-i\omega + \nu_t k^2) \mathbf{v}_k^{\perp}(\omega) = 0 \quad (11.150)$$

where

$$\nu_t = \frac{\eta}{m n_0} = \text{transverse kinetic viscosity.} \quad (11.150a)$$

(11.150) is satisfied by waves with the dispersion relation

$$\omega = -i\nu_t k^2 \quad (11.151)$$

These doubly degenerate modes are shear modes with eigenvectors lying in the plane perpendicular to the propagation direction  $\hat{\mathbf{k}}$ . Indeed, their behavior is similar to the diffusion mode  $\omega_0^{(2)}$  [ see (11.118) of §11.E.2 ]. Owing to the time dependence factor  $e^{-\nu_t k^2 t}$ , any short wavelength shear disturbance will damp out quickly.

The rest of the hydrodynamic equations deals only with the longitudinal modes.

$$i\omega n_k(\omega) - i n_0 k v_k^{\parallel}(\omega) = 0$$

$$i\omega m n_0 v_k^{\parallel}(\omega) = i \left( \frac{\partial P}{\partial n} \right)_T k n_k(\omega) + i \left( \frac{\partial P}{\partial T} \right)_n k T_k(\omega) + \eta k^2 v_k^{\parallel}(\omega) + \left( \zeta + \frac{1}{3} \eta \right) k^2 v_k^{\parallel}(\omega)$$

$$i\omega m n_0 \left( \frac{\partial s}{\partial n} \right)_T n_k(\omega) + i\omega m n_0 \left( \frac{\partial s}{\partial T} \right)_n T_k(\omega) = \frac{K}{T_0} k^2 T_k(\omega)$$

A little rearrangement gives

$$\omega n_k(\omega) - n_0 k v_k^{\parallel}(\omega) = 0$$

$$-\left( \frac{\partial P}{\partial n} \right)_T \frac{k}{m n_0} n_k(\omega) + \left[ \omega + i \left( \zeta + \frac{4}{3} \eta \right) \frac{k^2}{m n_0} \right] v_k^{\parallel}(\omega) - \left( \frac{\partial P}{\partial T} \right)_n \frac{k}{m n_0} T_k(\omega) = 0$$

$$\omega \frac{\left( \frac{\partial s}{\partial n} \right)_T}{\left( \frac{\partial s}{\partial T} \right)_n} n_k(\omega) + \left( \omega + i \frac{K}{m n_0 \left( \frac{\partial s}{\partial T} \right)_n T_0} k^2 \right) T_k(\omega) = 0$$

Using the thermodynamic relations given in §10.C.1, we have [ caution:  $s = \frac{S}{M} = \tilde{s}$  there &  $s = \frac{S}{N} = \tilde{s} m$  here ]

$$\begin{aligned} \frac{1}{m} \left( \frac{\partial P}{\partial n} \right)_T &= \frac{c^2}{\gamma} & c &= \sqrt{\left( \frac{\partial P}{m \partial n} \right)_s^0} & \gamma &= \frac{c_P}{c_V} \\ \left( \zeta + \frac{4}{3} \eta \right) \frac{1}{m n_0} &= v_l & \left( \frac{\partial P}{\partial T} \right)_n &= \frac{m n_0 \alpha_P c^2}{\gamma} \\ \left( \frac{\partial s}{\partial n} \right)_T^0 &= -\frac{m \alpha_P c^2}{n_0 \gamma} & \left( \frac{\partial s}{\partial T} \right)_n^0 &= \frac{c_V}{T_0} & c_P &= c_V + \frac{m c^2 T_0 \alpha_P^2}{\gamma} \end{aligned}$$

Hence, the hydrodynamic equations become

$$\begin{aligned} \omega n_k(\omega) - n_0 k v_k''(\omega) &= 0 \\ -\frac{c^2}{\gamma} \frac{k}{n_0} n_k(\omega) + (\omega + i v_l k^2) v_k''(\omega) - \frac{\alpha_P c^2}{\gamma} k T_k(\omega) &= 0 \\ -\omega \frac{n_0 \gamma}{c_V T_0} n_k(\omega) + \left( \omega + i \frac{K}{n_0 c_V} k^2 \right) T_k(\omega) &= 0 \end{aligned}$$

or, in matrix form,

$$\begin{pmatrix} \omega & -n_0 k & 0 \\ -\frac{c^2}{\gamma} \frac{k}{n_0} & \omega + i v_l k^2 & -\frac{\alpha_P c^2}{\gamma} k \\ -\omega \frac{m \alpha_P c^2}{n_0 c_V \gamma} T_0 & 0 & \omega + i \gamma \chi k^2 \end{pmatrix} \begin{pmatrix} n_k(\omega) \\ v_k''(\omega) \\ T_k(\omega) \end{pmatrix} = 0 \quad (11.152)$$

where we have used (10.62) to write

$$\chi = \frac{K}{n_0 c_P} \quad \gamma \chi = \frac{K}{n_0 c_V} \quad (11.152a)$$

Non-trivial solutions to (11.152) are possible only if the determinant of the matrix  $\mathbb{M}(\omega)$  vanishes. The roots of

$$\det \mathbb{M}(\omega) = 0$$

thus give the normal mode dispersion relations.

Using the *Mathematica* code in §Code, we get

$$\omega_1 = -i \chi k^2 = -i \frac{K}{n_0 c_P} k^2 \quad (11.153)$$

[ Note: we have replaced  $c_p$  with  $c_V$  to avoid confusing with  $c_P$ . ]

$$\begin{aligned} \omega_{\pm} &= \pm c k - i \frac{\chi c_P - c_V (\chi - v_l)}{2 c_V} k^2 \\ &= \pm c k - i \frac{v_l + \chi (\gamma - 1)}{2} k^2 \end{aligned}$$

$$\begin{aligned}
&= \pm c k - i \frac{1}{2} \left[ v_l + \left( \frac{1}{c_V} - \frac{1}{c_P} \right) \frac{K}{n_0} \right] k^2 && \text{[(11.152a) used.]} \\
&= \pm c k - i \frac{1}{2 m n_0} \left[ \zeta + \frac{4}{3} \eta + m \left( \frac{1}{c_V} - \frac{1}{c_P} \right) K \right] k^2 && (11.154)
\end{aligned}$$

Owing to the  $k^2$  dependence, the  $\omega_1$  mode is diffusion-like and is therefore associated with the heat propagation (wave). Similarly, the  $k$  dependence means the  $\omega_{\pm}$  modes are sound waves. Together with the 2-fold degenerated shear wave frequency in (11.151), we have 5 normal mode frequencies for the dilute-gas-like system.

Including the diffusion frequency in (11.114), we get 6 normal mode frequencies for a 2-component system.

## Code

$$\text{In[1]:= } \mathbf{M} = \begin{pmatrix} \omega & -n_0 \mathbf{k} & \mathbf{0} \\ -\mathbf{A1} \mathbf{k} & \omega + \mathbf{i} \mathbf{B1} k^2 & -\mathbf{A3} \mathbf{k} \\ -\omega \mathbf{A2} & \mathbf{0} & \omega + \mathbf{i} \mathbf{B2} k^2 \end{pmatrix};$$

**sol = Solve[Det[M] == 0, ω];**

$$\text{In[3]:= } \omega \mathbf{s} = (\omega /. \text{sol}) + \mathbf{0}[k]^3$$

$$\begin{aligned}
\text{Out[3]= } & \left\{ \left( \frac{\left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{1/6}}{\sqrt{3}} + \frac{\mathbf{A1} n_0 + \mathbf{A2} \mathbf{A3} n_0}{\sqrt{3} \left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{1/6}} \right) \mathbf{k} + \left( -\frac{1}{3} \mathbf{i} (\mathbf{B1} + \mathbf{B2}) + \right. \\
& \left. \left( \mathbf{i} (\mathbf{A1} + \mathbf{A2} \mathbf{A3}) (\mathbf{A1} \mathbf{B1} + \mathbf{A2} \mathbf{A3} \mathbf{B1} - 2 \mathbf{A1} \mathbf{B2} + \mathbf{A2} \mathbf{A3} \mathbf{B2}) n_0^2 \right) / \left( 6 \left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{2/3} \right) - \right. \\
& \left. \left( \mathbf{i} (\mathbf{A1} \mathbf{B1} n_0 + \mathbf{A2} \mathbf{A3} \mathbf{B1} n_0 - 2 \mathbf{A1} \mathbf{B2} n_0 + \mathbf{A2} \mathbf{A3} \mathbf{B2} n_0) \right) / \left( 6 \left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{1/3} \right) \right\} k^2 + \mathbf{O}[k]^3, \\
& \left( -\frac{\left( 1 - \mathbf{i} \sqrt{3} \right) \left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{1/6}}{2 \sqrt{3}} - \frac{\mathbf{i} \left( -\mathbf{i} + \sqrt{3} \right) (\mathbf{A1} n_0 + \mathbf{A2} \mathbf{A3} n_0)}{2 \sqrt{3} \left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{1/6}} \right) \mathbf{k} + \\
& \left( -\frac{1}{3} \mathbf{i} (\mathbf{B1} + \mathbf{B2}) + \left( \left( -\mathbf{i} + \sqrt{3} \right) (\mathbf{A1} + \mathbf{A2} \mathbf{A3}) (\mathbf{A1} \mathbf{B1} + \mathbf{A2} \mathbf{A3} \mathbf{B1} - 2 \mathbf{A1} \mathbf{B2} + \mathbf{A2} \mathbf{A3} \mathbf{B2}) n_0^2 \right) / \right. \\
& \left. \left( 12 \left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{2/3} \right) + \left( \left( \mathbf{i} + \sqrt{3} \right) (\mathbf{A1} \mathbf{B1} n_0 + \mathbf{A2} \mathbf{A3} \mathbf{B1} n_0 - 2 \mathbf{A1} \mathbf{B2} n_0 + \mathbf{A2} \mathbf{A3} \mathbf{B2} n_0) \right) / \right. \\
& \left. \left( 12 \left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{1/3} \right) \right\} k^2 + \mathbf{O}[k]^3, \\
& \left( -\frac{\left( 1 + \mathbf{i} \sqrt{3} \right) \left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{1/6}}{2 \sqrt{3}} + \frac{\mathbf{i} \left( \mathbf{i} + \sqrt{3} \right) (\mathbf{A1} n_0 + \mathbf{A2} \mathbf{A3} n_0)}{2 \sqrt{3} \left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{1/6}} \right) \mathbf{k} + \\
& \left( -\frac{1}{3} \mathbf{i} (\mathbf{B1} + \mathbf{B2}) - \left( \left( \mathbf{i} + \sqrt{3} \right) (\mathbf{A1} + \mathbf{A2} \mathbf{A3}) (\mathbf{A1} \mathbf{B1} + \mathbf{A2} \mathbf{A3} \mathbf{B1} - 2 \mathbf{A1} \mathbf{B2} + \mathbf{A2} \mathbf{A3} \mathbf{B2}) n_0^2 \right) / \right. \\
& \left. \left( 12 \left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{2/3} \right) - \left( \left( -\mathbf{i} + \sqrt{3} \right) (\mathbf{A1} \mathbf{B1} n_0 + \mathbf{A2} \mathbf{A3} \mathbf{B1} n_0 - 2 \mathbf{A1} \mathbf{B2} n_0 + \mathbf{A2} \mathbf{A3} \mathbf{B2} n_0) \right) / \right. \\
& \left. \left( 12 \left( -(\mathbf{A1} + \mathbf{A2} \mathbf{A3})^3 n_0^3 \right)^{1/3} \right) \right\} k^2 + \mathbf{O}[k]^3 \}
\end{aligned}$$



In[4]:=  $\omega s$  // PowerExpand // FullSimplify

$$\text{Out[4]} = \left\{ \sqrt{A1 + A2 A3} \sqrt{n_\theta} k - \frac{i (A1 B1 + A2 A3 (B1 + B2)) k^2}{2 (A1 + A2 A3)} + O[k]^3, \right. \\ \left. -\sqrt{A1 + A2 A3} \sqrt{n_\theta} k - \frac{i (A1 B1 + A2 A3 (B1 + B2)) k^2}{2 (A1 + A2 A3)} + O[k]^3, -\frac{i A1 B2 k^2}{A1 + A2 A3} + O[k]^3 \right\}$$

In[5]:=  $\omega se = \omega s$  // PowerExpand // Simplify

$$\text{Out[5]} = \left\{ \sqrt{A1 + A2 A3} \sqrt{n_\theta} k - \frac{i (A1 B1 + A2 A3 (B1 + B2)) k^2}{2 (A1 + A2 A3)} + O[k]^3, \right. \\ \left. -\sqrt{A1 + A2 A3} \sqrt{n_\theta} k - \frac{i (A1 B1 + A2 A3 (B1 + B2)) k^2}{2 (A1 + A2 A3)} + O[k]^3, -\frac{i A1 B2 k^2}{A1 + A2 A3} + O[k]^3 \right\}$$

In[6]:=  $\text{par} = \left\{ A1 \rightarrow \frac{c^2}{\gamma n_\theta}, A2 \rightarrow \frac{m \alpha_p c^2 T_\theta}{n_\theta c_V \gamma}, A3 \rightarrow \frac{\alpha_p c^2}{\gamma}, B1 \rightarrow v_r, B2 \rightarrow \gamma \chi \right\};$

$\omega val = (\omega se /. \text{par}) // \text{PowerExpand} // \text{Simplify} // \text{Normal}$

$$\text{Out[7]} = \left\{ k \sqrt{n_\theta} \sqrt{\frac{c^2 (\gamma c_V + c^2 m T_\theta \alpha_p^2)}{\gamma^2 c_V n_\theta}} - \frac{i k^2 (\gamma c_V v_r + c^2 m T_\theta (\gamma \chi + v_r) \alpha_p^2)}{2 (\gamma c_V + c^2 m T_\theta \alpha_p^2)}, \right. \\ \left. -k \sqrt{n_\theta} \sqrt{\frac{c^2 (\gamma c_V + c^2 m T_\theta \alpha_p^2)}{\gamma^2 c_V n_\theta}} - \frac{i k^2 (\gamma c_V v_r + c^2 m T_\theta (\gamma \chi + v_r) \alpha_p^2)}{2 (\gamma c_V + c^2 m T_\theta \alpha_p^2)}, -\frac{i k^2 \gamma^2 \chi c_V}{\gamma c_V + c^2 m T_\theta \alpha_p^2} \right\}$$

In[11]:=  $\omega v = \left( \omega val /. \alpha_p \rightarrow \sqrt{\frac{\gamma (c_p - c_V)}{c^2 m T_\theta}} \right) /. \gamma \rightarrow \frac{c_p}{c_V} // \text{Simplify} // \text{PowerExpand}$

$$\text{Out[11]} = \left\{ \frac{k (-i k \chi c_p + c_V (2 c + i k (\chi - v_r)))}{2 c_V}, -\frac{i k (k \chi c_p + c_V (-2 i c + k (-\chi + v_r)))}{2 c_V}, -i k^2 \chi \right\}$$