

11.G.3. Thermal Conductivity

Applying the same procedure in §11.G.2 to (11.192), we set [c.f. (11.202)]

$$A_x(\mathbf{p}) = \sum_{l=0}^{\infty} a_l p_x S'_q \left(\beta \frac{p^2}{2m} \right) \quad (11.212)$$

Putting (11.212) into (11.192) gives

$$\begin{aligned} K &= -\frac{n_0 k_B}{m^2} \left(\frac{\beta}{2\pi m} \right)^{3/2} \sum_{l=0}^{\infty} a_l \int d\mathbf{p} e^{-\beta p^2/2m} \left(-\frac{5}{2} + \frac{\beta}{2m} p^2 \right) p_x^2 S'_q \left(\beta \frac{p^2}{2m} \right) \\ &= \frac{n_0 k_B}{m^2} \left(\frac{\beta}{2\pi m} \right)^{3/2} \sum_{l=0}^{\infty} a_l \int d\mathbf{p} e^{-\beta p^2/2m} p_x^2 S_{3/2}^1 \left(\beta \frac{p^2}{2m} \right) S'_q \left(\beta \frac{p^2}{2m} \right) \quad [(11.200) \text{ used.}] \end{aligned}$$

Using (11.202b), we get

$$K = \frac{n_0 k_B}{m^2} \left(\frac{\beta}{2\pi m} \right)^{3/2} \sum_{l=0}^{\infty} a_l \frac{4\pi}{3} \int_0^{\infty} dp e^{-\beta p^2/2m} p^4 S_{3/2}^1 \left(\beta \frac{p^2}{2m} \right) S'_q \left(\beta \frac{p^2}{2m} \right) \quad (11.212a)$$

Setting $q = \frac{3}{2}$, we can use (11.202a) to write (11.212a) as

$$\begin{aligned} K &= \frac{n_0 k_B}{m^2} \left(\frac{\beta}{2\pi m} \right)^{3/2} \frac{4\pi}{3} \left(\frac{m}{\beta} \right)^{5/2} 2^{3/2} \sum_{l=0}^{\infty} a_l \langle S_{3/2}^1 | S'_{3/2} \rangle_{3/2} \\ &= \frac{4 n_0 k_B}{3 m \beta \sqrt{\pi}} \sum_{l=0}^{\infty} a_l \delta_{l,1} \frac{\Gamma\left(\frac{5}{2} + l\right)}{l!} \\ &= \frac{4 n_0 k_B}{3 m \beta \sqrt{\pi}} a_1 \Gamma\left(\frac{7}{2}\right) \\ &= \frac{5 n_0 k_B}{2 m \beta} a_1 \end{aligned} \quad (11.213)$$

Gamma [7/2]

$$\frac{15 \sqrt{\pi}}{8}$$

In order to calculate a_1 , we put (11.212) into (11.195) and get

$$\hat{C}^+ A_x = \sum_{l=0}^{\infty} a_l \hat{C}^+ \left[p_x S'_{3/2} \left(\beta \frac{p^2}{2m} \right) \right] = -S_{3/2}^1 \left(\beta \frac{p^2}{2m} \right) p_x \quad (11.204a)$$

Using (11.202d), we see that $\left(\frac{\beta}{2\pi m} \right)^{3/2} \int d\mathbf{p} e^{-\beta p^2/2m} p_x S'_{3/2} \left(\beta \frac{p^2}{2m} \right) \times (11.204a)$ gives

$$\begin{aligned} \sum_{l=0}^{\infty} M_{l,1} a_l &= -\frac{4m}{3\sqrt{\pi}\beta} \langle S'_{3/2} | S_{3/2}^1 \rangle_{3/2} \\ &= -\frac{4m}{3\sqrt{\pi}\beta} \delta_{l,1} \Gamma\left(\frac{7}{2}\right) \end{aligned}$$

$$= -\frac{5m}{2\beta} \delta_{l',1} \quad (11.214)$$

where

$$M_{l'l'} = \left(\frac{\beta}{2\pi m} \right)^{3/2} \int d\mathbf{p} e^{-\beta p^2/2m} p_x S'_{3/2} \left(\beta \frac{p^2}{2m} \right) \hat{C}^+ \left[p_x S'_{3/2} \left(\beta \frac{p^2}{2m} \right) \right] \quad (11.215)$$

$$= \left\langle p_x S'_{3/2} \left(\beta \frac{p^2}{2m} \right), \hat{C}^+ \left[p_x S'_{3/2} \left(\beta \frac{p^2}{2m} \right) \right] \right\rangle$$

$$= \left\langle p_x S'_{3/2} \hat{C}^+ (p_x S'_{3/2}) \right\rangle_{\beta} \quad (11.215a)$$

In matrix form, (11.214) becomes

$$\mathbb{M} \mathbf{a} = \begin{pmatrix} M_{00} & M_{01} & M_{02} & \cdots \\ M_{10} & M_{11} & M_{12} & \cdots \\ M_{20} & M_{21} & M_{22} & \cdots \\ \vdots & \vdots & \vdots & \ddots \end{pmatrix} \begin{pmatrix} a_0 \\ a_1 \\ a_2 \\ \vdots \end{pmatrix} = -\frac{5m}{2\beta} \begin{pmatrix} 0 \\ 1 \\ 0 \\ \vdots \end{pmatrix} \quad (11.215b)$$

(11.214) can be solved by truncating the sum at $l = \nu$ to give

$$\sum_{l=0}^{\nu} M_{l'l}^{(\nu)} a_l^{(\nu)} = -\frac{5m}{2\beta} \delta_{l',1} \quad l' = 0, 1, \dots, \nu \quad (11.215c)$$

The corresponding matrix form is the $(\nu + 1)$ -dimensional version of (11.215b)

$$\mathbb{M}^{(\nu)} \mathbf{a}^{(\nu)} = -\frac{5m}{2\beta} \mathbf{j}^{(\nu)} \quad (11.215d)$$

Using (11.215a), we have, since p_x is the eigenfunction of the zero eigenvalue of the self-adjoint operator \hat{C}^+ [see (11.159)],

$$M_{00} = \langle p_x, \hat{C}^+ p_x \rangle = 0$$

$$M_{01} = \langle p_x, \hat{C}^+ (p_x S'_{3/2}) \rangle = \langle \hat{C}^+ p_x, p_x S'_{3/2} \rangle = 0 = M_{10} \quad (11.215e)$$

so that the lowest order non-trivial form of (11.215d) is for $\nu = 1$,

$$\begin{pmatrix} 0 & 0 \\ 0 & M_{11} \end{pmatrix} \begin{pmatrix} a_0 \\ a_1 \end{pmatrix} = -\frac{5m}{2\beta} \begin{pmatrix} 0 \\ 1 \end{pmatrix}$$

→ $a_0 = 0$

$$a_1 = -\frac{5m}{2\beta M_{11}} \quad (11.215f)$$

(11.213) then gives

$$K = -\frac{25 n_0 k_B}{4 \beta^2 M_{11}}$$

$$= -\frac{25 n_0 k_B}{4 \beta^2 \langle p_x S'_{3/2} \hat{C}^+ (p_x S'_{3/2}) \rangle_{\beta}} \quad (11.217)$$

Using the results of Exercise 11.4 for a gas of hard spheres of radius R , we have

$$M_{11} = -\frac{64}{3} n_0 \frac{\sqrt{m\pi}}{\beta^{3/2}} R^2$$

$$\rightarrow K = \frac{75 k_B}{256 R^2} \sqrt{\frac{k_B T}{m \pi}} \quad (11.218)$$

Exercise 11.4

Evaluate M_{11} for a gas of hard spheres of radius R .

Answer

$$M_{11} = \left\langle p_x S_{3/2}^1 \hat{C}^+ (p_x S_{3/2}^1) \right\rangle_\beta \quad (5)$$

$$= \left\langle p_x \left(-\frac{5}{2} + \frac{\beta}{2m} p^2 \right), \hat{C}^+ \left[p_x \left(-\frac{5}{2} + \frac{\beta}{2m} p^2 \right) \right] \right\rangle$$

$$= \left\langle p_x \frac{\beta}{2m} p^2, \hat{C}^+ \left(p_x \frac{\beta}{2m} p^2 \right) \right\rangle \quad [\text{See (11.215e).}]$$

$$= \left(\frac{\beta}{2m} \right)^2 \left\langle p_x p^2 \hat{C}^+ (p_x p^2) \right\rangle_\beta \quad (6a)$$

Using (11.101) of §11.D.2, this becomes

$$M_{11} = -\frac{1}{4} n_0 \left(\frac{\beta}{2m} \right)^2 \left(\frac{\beta}{2\pi m} \right)^3 \int d\mathbf{p} \int d\mathbf{p}' e^{-\beta(p^2+p'^2)/2m} \int d\Omega v \sigma(b, v) \quad (6)$$

$$\times \left(p_{fx} p_f^2 - p_x p^2 + p_{fx}' p_f'^2 - p_x' p'^2 \right)^2$$

Switching to variables $(\mathbf{V}_{CM}, \mathbf{v})$ we have [see equations in between (11.210a & b)]

$$\mathbf{p} p^2 = m^3 \left(\mathbf{V}_{CM} - \frac{1}{2} \mathbf{v} \right)^3 = m^3 \left(V_{CM}^2 + \frac{1}{4} v^2 - \mathbf{V}_{CM} \cdot \mathbf{v} \right) \left(\mathbf{V}_{CM} - \frac{1}{2} \mathbf{v} \right)$$

$$\mathbf{p}_f p_f^2 = m^3 \left(\mathbf{V}_{CM} - \frac{1}{2} \mathbf{v}_f \right)^3 = m^3 \left(V_{CM}^2 + \frac{1}{4} v_f^2 - \mathbf{V}_{CM} \cdot \mathbf{v}_f \right) \left(\mathbf{V}_{CM} - \frac{1}{2} \mathbf{v}_f \right)$$

$$\mathbf{p}_f' p_f'^2 = m^3 \left(\mathbf{V}_{CM} + \frac{1}{2} \mathbf{v}_f \right)^3 = m^3 \left(V_{CM}^2 + \frac{1}{4} v_f^2 + \mathbf{V}_{CM} \cdot \mathbf{v}_f \right) \left(\mathbf{V}_{CM} + \frac{1}{2} \mathbf{v}_f \right)$$

$$\mathbf{p}' p'^2 = m^3 \left(\mathbf{V}_{CM} + \frac{1}{2} \mathbf{v} \right)^3 = m^3 \left(V_{CM}^2 + \frac{1}{4} v^2 + \mathbf{V}_{CM} \cdot \mathbf{v} \right) \left(\mathbf{V}_{CM} + \frac{1}{2} \mathbf{v} \right)$$

$$\rightarrow \mathbf{p}_f p_f^2 - \mathbf{p} p^2 + \mathbf{p}_f' p_f'^2 - \mathbf{p}' p'^2 = m^3 \left[(\mathbf{V}_{CM} \cdot \mathbf{v}_f) \mathbf{v}_f - (\mathbf{V}_{CM} \cdot \mathbf{v}) \mathbf{v} \right] \quad (7)$$

(6b) thus becomes

$$M_{11} = -\frac{1}{4} n_0 \left(\frac{\beta}{2m} \right)^2 \left(\frac{\beta}{2\pi m} \right)^3 m^{12} \int d\mathbf{V}_{CM} \int d\mathbf{v} e^{-\beta m (V_{CM}^2 + \frac{1}{4} v^2)} \quad (8)$$

$$\times \int d\Omega v \sigma(\Theta, v) \left[(\mathbf{V}_{CM} \cdot \mathbf{v}_f) v_{fx} - (\mathbf{V}_{CM} \cdot \mathbf{v}) v_x \right]^2$$

For an isotropic system such as the ideal-gas-like ones that the Boltzmann equation is designed for, we have

$$\left\langle p_j S_{3/2}^1 \hat{C}^+ (p_j S_{3/2}^1) \right\rangle_\beta = \frac{1}{3} \left\langle \mathbf{p} S_{3/2}^1 \cdot \hat{C}^+ (\mathbf{p} S_{3/2}^1) \right\rangle_\beta \quad \forall j = x, y, z$$

so that (8) can be written as

$$M_{11} = -\frac{1}{12} n_0 \left(\frac{\beta}{2m}\right)^2 \left(\frac{\beta}{2\pi m}\right)^3 m^{12} \int d\mathbf{V}_{CM} \int d\mathbf{v} e^{-\beta m (V_{CM}^2 + \frac{1}{4} v^2)} \quad (8a)$$

$$\times \int d\Omega v \sigma(\Theta, v) \left[(\mathbf{V}_{CM} \cdot \mathbf{v}_f) \mathbf{v}_f - (\mathbf{V}_{CM} \cdot \mathbf{v}) \mathbf{v} \right]^2$$

The \mathbf{V}_{CM} integral evaluates to

$$I_{CM} = \int d\mathbf{V}_{CM} e^{-\beta m V_{CM}^2} \left[(\mathbf{V}_{CM} \cdot \mathbf{v}_f) \mathbf{v}_f - (\mathbf{V}_{CM} \cdot \mathbf{v}) \mathbf{v} \right]^2$$

$$= \int d\mathbf{V}_{CM} e^{-\beta m V_{CM}^2} \left[(\mathbf{V}_{CM} \cdot \mathbf{v}_f)^2 v^2 + (\mathbf{V}_{CM} \cdot \mathbf{v})^2 v^2 - 2 (\mathbf{V}_{CM} \cdot \mathbf{v}_f) (\mathbf{V}_{CM} \cdot \mathbf{v}) \mathbf{v}_f \cdot \mathbf{v} \right]$$

Setting

$$\mathbf{v} = v(0, 0, 1) \quad \mathbf{v}_f = v(\sin\Theta, 0, \cos\Theta)$$

$$\mathbf{V}_{CM} = V(\sin\theta \cos\phi, \sin\theta \sin\phi, \cos\theta)$$

$$\rightarrow \mathbf{V}_{CM} \cdot \mathbf{v} = v V \cos\theta$$

$$\mathbf{V}_{CM} \cdot \mathbf{v}_f = v V (\sin\theta \cos\phi \sin\Theta + \cos\theta \cos\Theta)$$

we have

$$I_{CM} = \int_0^{2\pi} d\phi \int_0^\pi \sin\theta d\theta \int_0^\infty dV V^2 e^{-\beta m V^2} V^2 v^4 \left[(\sin\theta \cos\phi \sin\Theta + \cos\theta \cos\Theta)^2 \right.$$

$$\left. + \cos^2\theta - 2(\sin\theta \cos\phi \sin\Theta + \cos\theta \cos\Theta) \cos\theta \cos\Theta \right]$$

$$= v^4 \left(\frac{3\sqrt{\pi}}{8(m\beta)^{5/2}} \right) \left(\frac{8}{3} \pi \sin^2\Theta \right)$$

$$= \left(\frac{\pi}{m\beta} \right)^{5/2} v^4 \sin^2\Theta \quad (8b)$$

where

$$A1 = \int_0^{2\pi} \int_0^\pi \left((\sin[\theta] \cos[\phi] \sin[\Theta] + \cos[\theta] \cos[\Theta])^2 + \cos^2[\theta] - \right.$$

$$\left. 2(\sin[\theta] \cos[\phi] \sin[\Theta] + \cos[\theta] \cos[\Theta]) \cos[\theta] \cos[\Theta] \right) \sin[\theta] d\theta d\phi$$

$$\frac{8}{3} \pi \sin^2[\Theta]$$

$$A2 = \text{Assuming}[\beta > 0 \&\& m > 0, \int_0^\infty v^4 e^{-\beta m v^2} dv]$$

$$\frac{3\sqrt{\pi}}{8(m\beta)^{5/2}}$$

A1 A2

$$\frac{\pi^{3/2} \sin^2[\Theta]}{(m\beta)^{5/2}}$$

Putting (8b) into (8a) gives

$$M_{11} = -n_0 \frac{1}{384} \frac{m^{9/2} \beta^{5/2}}{\pi^{3/2}} \int d\mathbf{v} e^{-\beta m v^2/4} v^5 \int d\Omega \sigma(\Theta, v) \sin^2\Theta \quad (10a)$$

where

$$A3 = \frac{1}{12} \left(\frac{\beta}{2m} \right)^2 \left(\frac{\beta}{2\pi m} \right)^3 m^{12} A1 A2 // \text{PowerExpand}$$

$$\frac{m^{9/2} \beta^{5/2} \text{Sin}[\Phi]^2}{384 \pi^{3/2}}$$

For the hard sphere gas, $\sigma(\Theta, v) = R^2$ so that

$$\begin{aligned} \mathcal{T}_\Theta &= \int d\Omega \sigma(\Theta, v) \sin^2 \Theta \\ &= 2\pi R^2 \int_0^\pi d\Theta \sin^3 \Theta \\ &= \frac{8\pi}{3} R^2 \end{aligned}$$

where

$$\int_0^\pi \text{Sin}[\Theta]^3 d\Theta$$

$$\frac{4}{3}$$

(10a) thus becomes

$$\begin{aligned} M_{11} &= -\frac{n_0}{144} \frac{m^{9/2} \beta^{5/2}}{\sqrt{\pi}} R^2 \int d\mathbf{v} e^{-\beta m v^2/4} v^5 \\ &= -\frac{n_0}{144} \frac{m^{9/2} \beta^{5/2}}{\sqrt{\pi}} R^2 4\pi \int_0^\infty dv e^{-\beta m v^2/4} v^7 \\ &= -\frac{64}{3} n_0 \frac{\sqrt{m\pi}}{\beta^{3/2}} R^2 \end{aligned} \tag{11}$$

where

$$\frac{A3}{\text{Sin}[\Phi]^2} n_0 \frac{8\pi}{3} R^2$$

$$\frac{m^{9/2} R^2 \beta^{5/2} n_0}{144 \sqrt{\pi}}$$

$$M11 = \text{Assuming}[\beta > 0 \&\& m > 0, \frac{A3}{\text{Sin}[\Phi]^2} n_0 \frac{8\pi}{3} R^2 4\pi \int_0^\infty v^7 e^{-\beta m v^2/4} dv] // \text{PowerExpand}$$

$$\frac{64 \sqrt{m} \sqrt{\pi} R^2 n_0}{3 \beta^{3/2}}$$

$$\frac{25 n_0}{4 \beta^2} \frac{1}{M11}$$

$$\frac{75}{256 \sqrt{m} \sqrt{\pi} R^2 \sqrt{\beta}}$$