

## SI0.D. Thermoelectricity

Read Reichl's introductory remarks.

See §4.3 of O.Madelung, "Introduction to Solid State Theory" for the conventional approach.

**Thermal couple:** temperature measuring device consisting of joining two different metal bars to form a closed circuit of two junctions.

As the name implies, the subject **thermoelectricity** deals with the transport of charge (or heat) caused by a temperature gradient (or electric field). It is exemplified by the following phenomena.

**Seebeck effect:** temperature difference across the junction of two different metals creates an electromotive force (EMF).

**Peltier effect:** electric current creates temperature difference between the two junctions of a thermal couple.

**Thomson effect:** heat is emitted or absorbed if a current is passed through a wire maintained at a temperature gradient.

These effects are easily explained by treating a metal as a neutral system consisting of a fluid of electrons moving in a background of immobile positive ions.

Let

$\mu_{\text{el}} = \mu_{\text{el}}(T)$  = chemical potential of electrons

$\mu_{\text{el}}^e = \mu_{\text{el}} - F\phi$  = electrochemical potential of electrons

$\phi$  = electric potential                       $F$  = Faraday's constant

$\mathbf{J}_q$  = heat flux                                       $\mathbf{J}_{\text{el}}$  = electron flux

Since the thermoelectric effects usually involve two types of metal, temperature gradient, and electric field, we are dealing with an entropy production [see (10.179a)]

$$T\sigma = -\mathbf{J}_S \cdot \nabla_r T - \mathbf{J}_{\text{el}} \cdot \nabla_r \mu_{\text{el}}^e \quad [\text{molar version}] \quad (10.274)$$

$$= -\mathbf{J}_S \cdot \nabla_r T - \mathbf{J}_{\text{el}} \cdot (\nabla_r \mu_{\text{el}} - F\mathbf{E}) \quad (10.274a)$$

which corresponds to the generalized Ohm's law

$$\begin{pmatrix} \mathbf{J}_S \\ \mathbf{J}_{\text{el}} \end{pmatrix} = - \begin{pmatrix} L_{SS} & L_{SE} \\ L_{ES} & L_{EE} \end{pmatrix} \begin{pmatrix} \nabla_r T \\ \nabla_r \mu_{\text{el}}^e \end{pmatrix} \quad (10.275-6)$$

$$= - \begin{pmatrix} L_{SS} & L_{SE} \\ L_{ES} & L_{EE} \end{pmatrix} \begin{pmatrix} \nabla_r T \\ \nabla_r \mu_{\text{el}} - F\mathbf{E} \end{pmatrix} \quad (10.276a)$$

The Onsager's relations require

$$L_{SE} = L_{ES}$$

**Contact potential:** potential difference across the junction of two different metals.

### SI0.D.I. The Peltier Effect

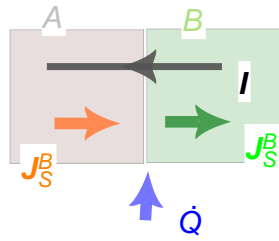


Fig.10.5a

Consider first a current passing from a metal wire of metal  $A$  into another of metal  $B$  [see Fig.10.5a]. If we keep a uniform temperature throughout the wires,  $\nabla T = 0$ , and (10.274-6) becomes, for each wire,

$$\begin{aligned}
 T \sigma &= -\mathbf{J}_{el} \cdot (\nabla_r \mu_{el} - F\mathbf{E}) \\
 \mathbf{J}_S &= -L_{SE} (\nabla_r \mu_{el} - F\mathbf{E}) \\
 \mathbf{J}_{el} &= -L_{EE} (\nabla_r \mu_{el} - F\mathbf{E}) \\
 \rightarrow \mathbf{J}_S &= \frac{L_{SE}}{L_{EE}} \mathbf{J}_{el} = -\frac{L_{SE}}{FL_{EE}} I \quad (10.279a)
 \end{aligned}$$

where

$$I = -F \mathbf{J}_{el} = \text{electric current density due to the electron flux.}$$

The **entropy transport parameter** ( or **Seebeck coefficient** ) is defined as

$$S^* = \frac{J_S}{J_{el}} = \frac{L_{SE}}{L_{EE}} \quad (10.279)$$

For two wires of the same uniform cross sections, all fluxes are perpendicular to the junction. Charge conservation demands

$$\mathbf{J}_{el}^A = \mathbf{J}_{el}^B = \mathbf{J}_{el}$$

so that (10.279a) gives

$$\mathbf{J}_S^A = S_A^* \mathbf{J}_{el} = -\frac{S_A^*}{F} I \quad \mathbf{J}_S^B = S_B^* \mathbf{J}_{el} = -\frac{S_B^*}{F} I$$

Thus,

$$\begin{aligned}
 S_A^* \neq S_B^* &\rightarrow \mathbf{J}_S^A \neq \mathbf{J}_S^B \\
 &\rightarrow \text{Heat is generated (or absorbed) at the junction}
 \end{aligned}$$

Let  $I$  be flowing from  $B$  to  $A$  and denote its magnitude as  $I_{BA}$ . Hence,

$$I = I_{BA} \hat{n}_{BA} \quad \mathbf{J}_S^A = -\frac{S_A^*}{F} I_{BA} \hat{n}_{BA} \quad \mathbf{J}_S^B = -\frac{S_B^*}{F} I_{BA} \hat{n}_{BA}$$

where  $\hat{n}_{BA}$  is the unit vector pointing from  $B$  to  $A$  across the junction.

If  $|\mathbf{J}_S^B| > |\mathbf{J}_S^A|$ , heat is absorbed at the junction. Let  $\dot{Q}$  be the rate of heat absorption per unit area.

Then

$$\dot{Q} = T (\mathbf{J}_S^B - \mathbf{J}_S^A) \cdot (-\hat{n}_{BA}) = \frac{T}{F} (S_B^* - S_A^*) I_{BA} \quad (10.279b)$$

where  $\dot{Q} > 0$  means heat is absorbed at the junction and  $\dot{Q} < 0$  means heat is emitted at the junction.

Note that  $\dot{Q}$  is a scalar with units

$$[\dot{Q}] = [\text{heat}/(\text{area} \cdot \text{time})]$$

Since the material labels are dummies, (10.279b) can be written in a more general form

$$\dot{Q} = \frac{T}{F} (S_j^* - S_k^*) I_{jk} \quad j, k = A, B \quad (10.279c)$$

for a junction with electric current flowing from metal  $j$  to  $k$ .

The **Peltier heat** is defined as

$$\bar{\pi} \equiv \left( \frac{\dot{Q}}{I} \right)_{\nabla T = 0} \quad (10.277)$$

= rate of heat absorption per unit area per unit electric current density

$$= \frac{T}{F} (S_j^* - S_k^*) \quad \text{for } I_{jk} \quad (10.280)$$

The **Peltier coefficient**  $\Pi$  is defined by

$$\dot{Q} = (\Pi_j - \Pi_k) I \quad (10.280a)$$

Comparing with (10.280) gives

$$\Pi_j = T S_j^* \quad (10.280b)$$

which is known as **Thomson's first relation**.

The circuit for measuring the Peltier effect is shown in Fig.10.5b. The heat absorption directions are for the case  $\dot{Q} > 0$ ,  $S_B^* < S_A^*$ .

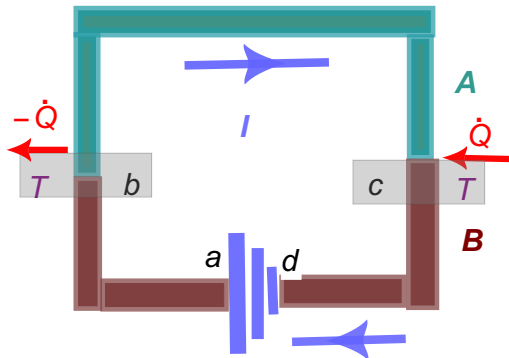


Fig.10.5b.

See Reich's Fig.10.5 for the experimental configurations for measuring the Peltier effect.

## S10.D.2. The Seebeck Effect

A typical circuit for measuring the Seebeck effect is shown in Fig.10.6. The two junctions,  $b$  &  $c$ , between the wires of different metals,  $A$  &  $B$ , are kept at different temperatures  $T$  &  $T + \Delta T$ . The circuit is open so that the potential at points  $a$  &  $d$  can be measured by a potentiometer at temperature  $T_0$ .

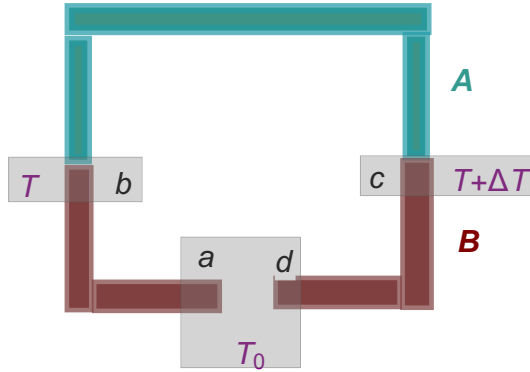


Fig.10.6.

Setting  $J_{el} = 0$  in (10.274-6) gives

$$T \sigma = -J_S \cdot \nabla_r T$$

$$J_S = -L_{SS} \nabla_r T - L_{SE} \nabla_r \mu_{el}^e$$

$$0 = -L_{ES} \nabla_r T - L_{EE} \nabla_r \mu_{el}^e$$

$$\begin{aligned} \rightarrow \nabla_r \mu_{el}^e &= -\frac{L_{ES}}{L_{EE}} \nabla_r T \\ &= -\frac{L_{SE}}{L_{EE}} \nabla_r T && \text{[ Onsager's relations used. ]} \\ &= -S^* \nabla_r T && \text{[ (10.279) used. ]} \end{aligned} \tag{10.281}$$

Integrating along the circuit from point  $a$  to  $d$  gives

$$\int_a^d d\mathbf{r} \cdot \nabla_r \mu_{el}^e = \int_a^d d\mu_{el}^e = (\mu_{el} - F\phi)_a^d = -F(\phi_d - \phi_a) \tag{10.282a}$$

$$= -\int_a^d d\mathbf{r} \cdot S^* \nabla_r T \quad \text{[ (10.281) used. ]}$$

$$= -\left[ \int_a^b dT S_B^* + \int_b^c dT S_A^* + \int_c^d dT S_B^* \right]$$

$$= -\left[ \int_{T_0}^T dT S_B^* + \int_T^{T+\Delta T} dT S_A^* + \int_{T+\Delta T}^{T_0} dT S_B^* \right]$$

$$= -\left[ \int_{T+\Delta T}^T dT S_B^* + \int_T^{T+\Delta T} dT S_A^* \right]$$

$$= \int_T^{T+\Delta T} dT (S_B^* - S_A^*) \tag{10.285}$$

$$\rightarrow \phi_{ad} = \phi_a - \phi_d = \frac{1}{F} \int_T^{T+\Delta T} dT (S_B^* - S_A^*) \tag{10.286}$$

$$\begin{aligned} \therefore \frac{d\phi_{ad}}{dT} &= \frac{S_B^* - S_A^*}{F} \\ &= \frac{\bar{\pi}}{T} && \text{[ (10.280) used. ]} \end{aligned} \tag{10.287}$$

Since (10.287) was obtained using Onsager's relations [see derivation of (10.281)], checking it against experimental data provides a test on the Onsager relations. Excellent agreement can be found in Reichl's Table 10.6.

### SI0.D.3. Thomson Heat

Since the Thomson effect involves only one type of metal subject to both a temperature gradient and an electric field, (10.274-6) become

$$T \sigma = -\mathbf{J}_S \cdot \nabla_r T + F \mathbf{J}_{el} \cdot \mathbf{E} \quad (10.288a)$$

which corresponds to the generalized Ohm's law

$$\begin{pmatrix} \mathbf{J}_S \\ \mathbf{J}_{el} \end{pmatrix} = - \begin{pmatrix} L_{SS} & L_{SE} \\ L_{ES} & L_{EE} \end{pmatrix} \begin{pmatrix} \nabla_r T \\ -F\mathbf{E} \end{pmatrix} = \begin{pmatrix} -L_{SS} \nabla_r T + L_{SE} F\mathbf{E} \\ -L_{ES} \nabla_r T + L_{EE} F\mathbf{E} \end{pmatrix} \quad (10.288b)$$

Eliminating  $\mathbf{E}$  gives

$$\begin{aligned} L_{EE} \mathbf{J}_S - L_{SE} \mathbf{J}_{el} &= -(L_{EE} L_{SS} - L_{SE} L_{ES}) \nabla_r T \\ \rightarrow \mathbf{J}_S &= \frac{L_{SE}}{L_{EE}} \mathbf{J}_{el} - \frac{\mathcal{L}}{L_{EE}} \nabla_r T \quad \mathcal{L} = L_{EE} L_{SS} - L_{SE} L_{ES} = \det \mathbb{L} \\ &= S^* \mathbf{J}_{el} - \frac{\mathcal{L}}{L_{EE}} \nabla_r T \end{aligned} \quad (10.288c)$$

Putting this into the entropy balance equation

$$\begin{aligned} \frac{\partial s}{\partial t} + \nabla_r \cdot \mathbf{J}_S &= 0 \\ \rightarrow \frac{\partial s}{\partial t} &= -S^* \nabla_r \cdot \mathbf{J}_{el} - \mathbf{J}_{el} \cdot \nabla_r S^* + \nabla_r \cdot \left( \frac{\mathcal{L}}{L_{EE}} \nabla_r T \right) \end{aligned}$$

where  $s$  is the entropy density.

Since  $S^*$  is a function of  $T$ , the 2nd term on the right corresponds to a heat generation

$$\dot{q} = -T \frac{dS^*}{dT} \mathbf{J}_{el} \cdot \nabla_r T \quad (10.288d)$$

which is called the **Thomson heat rate** since it is non-zero only when both an electric current and temperature gradient are present (conditions for the Thomson effect).

The **Thomson's coefficient**  $K$  is defined by

$$\dot{q} = -K \mathbf{J}_{el} \cdot \nabla_r T \quad (10.288e)$$

Comparing with (10.288d) gives

$$K = T \frac{dS^*}{dT} \quad (10.288f)$$

which is known as the **Thomson's second relation**.

Consider a wire of length  $L$  and cross section  $A$ . For small temperature difference  $\Delta T$  between the ends of the wire, (10.288e) can be written as

$$\begin{aligned} \dot{q} &= -K \frac{I}{A} \frac{\Delta T}{L} \\ \rightarrow \dot{Q} &= -K I \Delta T = \text{total heat rate of wire} \end{aligned}$$

$$\begin{aligned} \sigma_A &= \frac{1}{I} \lim_{\Delta T \rightarrow 0} \frac{\dot{Q}}{\Delta T} \\ &= \frac{1}{I} \frac{d\dot{Q}}{dT} \end{aligned} \quad (10.288)$$

is called by Reichl the Thomson heat.