

SI0.H.2. Sound Modes

To obtain the sound mode, we set all dissipative terms to zero and keep only $O(\Delta X)$ terms for any dynamic variable $X = X_0 + \Delta X$, where X_0 is its equilibrium value.

The balance (or hydrodynamic) equations (10.388, 89, 91) become

$$\frac{\partial \Delta \rho}{\partial t} + \rho_n^0 \nabla_r \cdot \mathbf{v}_n + \rho_s^0 \nabla_r \cdot \mathbf{v}_s = 0 \quad (10.411)$$

$$\rho_n^0 \frac{\partial \mathbf{v}_n}{\partial t} + \rho_s^0 \frac{\partial \mathbf{v}_s}{\partial t} + \nabla_r \Delta P = 0 \quad (10.412)$$

$$\rho^0 \frac{\partial \Delta s}{\partial t} + s^0 \frac{\partial \Delta \rho}{\partial t} + \rho^0 s^0 \nabla_r \cdot \mathbf{v}_n = 0 \quad (10.413)$$

Similarly, (10.392) simplifies to

$$\frac{\partial \mathbf{v}_s}{\partial t} + \nabla_r \Delta \tilde{\mu}_s = 0 \quad (10.414)$$

Choosing $\Delta \rho$ & ΔT as the independent thermodynamic variables, we have

$$\begin{aligned} d\Delta P &= \left(\frac{\partial P}{\partial \rho} \right)_T d\Delta \rho + \left(\frac{\partial P}{\partial T} \right)_\rho d\Delta T \\ \rightarrow \nabla_r \Delta P &= \frac{1}{\rho^0 \kappa_T} \nabla_r \Delta \rho + \left(\frac{\partial P}{\partial T} \right)_\rho \nabla_r \Delta T \end{aligned} \quad (10.414a)$$

where

$$\kappa_T = -\frac{1}{V} \left(\frac{\partial V}{\partial P} \right)_T = \frac{1}{\rho} \left(\frac{\partial \rho}{\partial P} \right)_T = \text{isothermal compressibility.} \quad (10.414b)$$

Similarly,

$$\begin{aligned} d\Delta s &= \left(\frac{\partial s}{\partial \rho} \right)_T d\Delta \rho + \left(\frac{\partial s}{\partial T} \right)_\rho d\Delta T \\ \rightarrow \frac{\partial \Delta s}{\partial t} &= -\frac{1}{\rho^2} \left(\frac{\partial P}{\partial T} \right)_V \frac{\partial \Delta \rho}{\partial t} + \frac{\tilde{c}_\rho}{T} \frac{\partial \Delta T}{\partial t} \end{aligned} \quad (10.414c)$$

where

$$\tilde{c}_\rho = T \left(\frac{\partial s}{\partial T} \right)_\rho = \text{specific heat at constant } \rho$$

and we have used the Maxwell relation

$$\left(\frac{\partial s}{\partial \rho} \right)_T = \left(\frac{\partial SIM}{\partial MIV} \right)_T = -\frac{V^2}{M^2} \left(\frac{\partial S}{\partial V} \right)_T = -\frac{1}{\rho^2} \left(\frac{\partial P}{\partial T} \right)_V \quad [M = \text{const}]$$

From the linearized Gibbs-Duhem equation (10.398a),

$$\rho s dT - dP + \rho_n d\tilde{\mu} + \rho_s d\tilde{\mu}_s = 0$$

we have

$$\rho^0 s^0 d\Delta T - d\Delta P + \rho_n^0 d\Delta \tilde{\mu} + \rho_s^0 d\Delta \tilde{\mu}_s = 0 \quad (10.414d)$$

For sound waves in a static He^4 fluid in contact with a heat reservoir of temperature T_0 , we can assume the normal & super components in a fluid element to be always in (local) equilibrium with each other.

Hence,

$$\tilde{\mu}(\mathbf{r}, t) = \tilde{\mu}_s(\mathbf{r}, t) \quad \rightarrow \quad d\tilde{\mu} = d\tilde{\mu}_s$$

so that (10.414d) simplifies to

$$\rho^0 s^0 d\Delta T - d\Delta P + \rho^0 d\Delta\tilde{\mu} = 0 \quad (10.414e)$$

$$\rightarrow \left(\frac{\partial \tilde{\mu}}{\partial P} \right)_T = \frac{1}{\rho^0} \quad \left(\frac{\partial \tilde{\mu}}{\partial T} \right)_P = -s^0 \quad (10.414f)$$

$$\left(\frac{\partial \tilde{\mu}}{\partial \rho} \right)_T = \frac{1}{\rho^0} \left(\frac{\partial P}{\partial \rho} \right)_T = \frac{1}{(\rho^0)^2 \kappa_T} \quad [(10.414b) \text{ used. }] \quad (10.414g)$$

and

$$\nabla_r \Delta P = \rho^0 s^0 \nabla_r \Delta T + \rho^0 \nabla_r \Delta\tilde{\mu} \quad (10.414h)$$

Thus,

$$\begin{aligned} d\Delta\tilde{\mu} &= \left(\frac{\partial \tilde{\mu}}{\partial \rho} \right)_T d\Delta\rho + \left(\frac{\partial \tilde{\mu}}{\partial T} \right)_\rho d\Delta T \\ &= \frac{1}{(\rho^0)^2 \kappa_T} d\Delta\rho + \left[\left(\frac{\partial \tilde{\mu}}{\partial T} \right)_P + \left(\frac{\partial \tilde{\mu}}{\partial P} \right)_T \left(\frac{\partial P}{\partial T} \right)_\rho \right] d\Delta T \quad [(2.8) \text{ used. }] \\ &= \frac{1}{(\rho^0)^2 \kappa_T} d\Delta\rho + \left[-s^0 + \frac{1}{\rho^0} \left(\frac{\partial P}{\partial T} \right)_\rho \right] d\Delta T \end{aligned} \quad (10.414i)$$

Putting (10.414i) into (10.414h) gives

$$\nabla_r \Delta P = \frac{1}{\rho^0 \kappa_T} \nabla_r \Delta\rho + \left(\frac{\partial P}{\partial T} \right)_\rho \nabla_r \Delta T \quad (10.414j)$$

(10.411-4) then become

$$\frac{\partial \Delta\rho}{\partial t} + \rho_n^0 \nabla_r \cdot \mathbf{v}_n + \rho_s^0 \nabla_r \cdot \mathbf{v}_s = 0 \quad [\text{unchanged}] \quad (10.415)$$

$$\rho_n^0 \frac{\partial \mathbf{v}_n}{\partial t} + \rho_s^0 \frac{\partial \mathbf{v}_s}{\partial t} + \frac{1}{\rho^0 \kappa_T} \nabla_r \Delta\rho + \left(\frac{\partial P}{\partial T} \right)_\rho \nabla_r \Delta T = 0 \quad [(10.414j) \text{ used.}] \quad (10.416)$$

$$\left[s^0 - \frac{1}{\rho^0} \left(\frac{\partial P}{\partial T} \right)_\rho \right] \frac{\partial \Delta\rho}{\partial t} + \frac{\rho^0 \tilde{c}_\rho}{T} \frac{\partial \Delta T}{\partial t} + \rho^0 s^0 \nabla_r \cdot \mathbf{v}_n = 0 \quad [(10.414c) \text{ used.}] \quad (10.417)$$

$$\frac{\partial \mathbf{v}_s}{\partial t} + \frac{1}{(\rho^0)^2 \kappa_T} \nabla_r \Delta\rho + \left[-s^0 + \frac{1}{\rho^0} \left(\frac{\partial P}{\partial T} \right)_\rho \right] \nabla_r \Delta T = 0 \quad [(10.414i) \text{ used.}] \quad (10.418)$$

Taking the Laplace transform in time & Fourier transform in space is equivalent to the following substitution rules:

$$\begin{aligned} f(\mathbf{r}, t) &\rightarrow \tilde{f}(\mathbf{k}, z) \\ \nabla_r f(\mathbf{r}, t) &\rightarrow i\mathbf{k} \tilde{f}(\mathbf{k}, z) \\ \frac{\partial}{\partial t} f(\mathbf{r}, t) &\rightarrow z \tilde{f}(\mathbf{k}, z) - f(\mathbf{k}, t=0) \end{aligned}$$

(10.415-8) can then be represented in matrix form as

$$\begin{aligned}
& \begin{pmatrix} z & 0 & ik\rho_n^0 & ik\rho_s^0 \\ \frac{ik}{\rho^0 \kappa_T} & ik\left(\frac{\partial P}{\partial T}\right)_\rho & z\rho_n^0 & z\rho_s^0 \\ z\left[s^0 - \frac{1}{\rho^0}\left(\frac{\partial P}{\partial T}\right)_\rho\right] & z\frac{\rho^0 \tilde{c}_\rho}{T} & ik\rho^0 s^0 & 0 \\ \frac{ik}{(\rho^0)^2 \kappa_T} & ik\left[-s^0 + \frac{1}{\rho^0}\left(\frac{\partial P}{\partial T}\right)_\rho\right] & 0 & z \end{pmatrix} \begin{pmatrix} \tilde{\rho}(\mathbf{k}, z) \\ \tilde{T}(\mathbf{k}, z) \\ \tilde{\mathbf{v}}_n(\mathbf{k}, z) \\ \tilde{\mathbf{v}}_s(\mathbf{k}, z) \end{pmatrix} \\
& = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & \rho_n^0 & \rho_s^0 \\ s^0 - \frac{1}{\rho^0}\left(\frac{\partial P}{\partial T}\right)_\rho & \frac{\rho^0 \tilde{c}_\rho}{T} & 0 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \Delta\rho(\mathbf{k}, 0) \\ \Delta T(\mathbf{k}, 0) \\ \mathbf{v}_n(\mathbf{k}, 0) \\ \mathbf{v}_s(\mathbf{k}, 0) \end{pmatrix} \tag{10.419}
\end{aligned}$$

Let

$$\mathbb{S}(\mathbf{k}, z) = \begin{pmatrix} z & 0 & ik\rho_n^0 & ik\rho_s^0 \\ \frac{ik}{\rho^0 \kappa_T} & ik\left(\frac{\partial P}{\partial T}\right)_\rho & z\rho_n^0 & z\rho_s^0 \\ z\left[s^0 - \frac{1}{\rho^0}\left(\frac{\partial P}{\partial T}\right)_\rho\right] & z\frac{\rho^0 \tilde{c}_\rho}{T} & ik\rho^0 s^0 & 0 \\ \frac{ik}{(\rho^0)^2 \kappa_T} & ik\left[-s^0 + \frac{1}{\rho^0}\left(\frac{\partial P}{\partial T}\right)_\rho\right] & 0 & z \end{pmatrix} \tag{10.420}$$

Starting at equilibrium, the right hand side of (10.419) vanishes and we have

$$\mathbb{S}(\mathbf{k}, z) \begin{pmatrix} \tilde{\rho}(\mathbf{k}, z) \\ \tilde{T}(\mathbf{k}, z) \\ \tilde{\mathbf{v}}_n(\mathbf{k}, z) \\ \tilde{\mathbf{v}}_s(\mathbf{k}, z) \end{pmatrix} = 0 \tag{10.420a}$$

The condition for (10.420a) to have non-trivial solutions is

$$\det \mathbb{S}(\mathbf{k}, z) = 0 \tag{10.421}$$

Now, the thermal expansivity α_P is very small for He⁴ fluid at low temperatures. Thus,

$$\begin{aligned}
\alpha_P &\equiv \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_P \approx 0 \\
&= -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial T} \right)_P = -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial P} \right)_T \left(\frac{\partial P}{\partial T} \right)_\rho = -\kappa_T \left(\frac{\partial P}{\partial T} \right)_\rho
\end{aligned}$$

$$\rightarrow \left(\frac{\partial P}{\partial T} \right)_\rho \approx 0$$

(10.420) thus simplifies to

$$\mathbf{S}(\mathbf{k}, z) \approx \begin{pmatrix} z & 0 & i\mathbf{k} \rho_n^0 & i\mathbf{k} \rho_s^0 \\ \frac{i\mathbf{k}}{\rho^0 \kappa_T} & 0 & z \rho_n^0 & z \rho_s^0 \\ z s^0 & z \frac{\rho^0 \tilde{c}_\rho}{T} & i\mathbf{k} \rho^0 s^0 & 0 \\ \frac{i\mathbf{k}}{(\rho^0)^2 \kappa_T} & -i\mathbf{k} s^0 & 0 & z \end{pmatrix} \quad (10.421a)$$

Using the *Mathematica* code in §Code, we get

$$\begin{aligned} \det \mathbf{S}(\mathbf{k}, z) &\approx -\frac{1}{\kappa_T T^0} (k^2 + \rho^0 \kappa_T z^2) \left[k^2 \rho_s^0 (s^0)^2 T^0 + \tilde{c}_\rho \rho_n^0 z^2 \right] \\ &= -\frac{\rho^0 \tilde{c}_\rho \rho_n^0}{T^0} \left(\frac{k^2}{\rho^0 \kappa_T} + z^2 \right) \left[\frac{k^2 \rho_s^0 (s^0)^2 T^0}{\tilde{c}_\rho \rho_n^0} + z^2 \right] \end{aligned} \quad (10.423)$$

The roots

$$z = \pm \frac{i\mathbf{k}}{\sqrt{\rho^0 \kappa_T}} \quad (10.423a)$$

correspond to waves with dispersion

$$\omega = \frac{k}{\sqrt{\rho^0 \kappa_T}}$$

and hence speed

$$c_1 = \frac{1}{\sqrt{\rho^0 \kappa_T}} \quad (10.424)$$

As shown on §Code, putting (10.423a) back into (10.420a) gives a solution of the form

$$\begin{pmatrix} \tilde{\rho}(\mathbf{k}, z) \\ \tilde{T}(\mathbf{k}, z) \\ \tilde{\mathbf{v}}_n(\mathbf{k}, z) \\ \tilde{\mathbf{v}}_s(\mathbf{k}, z) \end{pmatrix} = \begin{pmatrix} 1 \\ a_T \\ a_n \\ a_s \end{pmatrix} \tilde{\rho}(\mathbf{k}, z) \quad a_j = \text{const}$$

which means these waves are density (or sound) waves. Indeed, (10.424) is actually the speed of sound propagation in normal fluids since $\kappa_T \approx \kappa_S$ if $\left(\frac{\partial P}{\partial T} \right)_\rho \approx 0$ [see §10.C]. These waves are usually called the **first sound**.

The roots

$$z = \pm i\mathbf{k} s^0 \sqrt{\frac{\rho_s^0 T^0}{\tilde{c}_\rho \rho_n^0}} \quad (10.423b)$$

correspond to waves with dispersion

$$\omega = k s^0 \sqrt{\frac{\rho_s^0 T^0}{\tilde{c}_\rho \rho_n^0}}$$

and hence speed

$$c_2 = s^0 \sqrt{\frac{\rho_s^0 T^0}{\tilde{c}_p \rho_n^0}} \quad (10.425)$$

As shown on §Code, putting (10.423b) back into (10.420a) gives a solution of the form

$$\begin{pmatrix} \tilde{\rho}(\mathbf{k}, z) \\ \tilde{T}(\mathbf{k}, z) \\ \tilde{\mathbf{v}}_n(\mathbf{k}, z) \\ \tilde{\mathbf{v}}_s(\mathbf{k}, z) \end{pmatrix} = \begin{pmatrix} 0 \\ 1 \\ b_n \\ b_s \end{pmatrix} \tilde{T}(\mathbf{k}, z) \quad b_j = \text{const}$$

which means these waves are temperature waves. Owing to the linear dispersion relation, these waves are usually called the **second sound**.

Note that

$$c_2 = 0 \quad \text{if} \quad \rho_s^0 = 0$$

so that there is no second sound above the λ -point of the He I-He II phases [see Fig.10.15 in Reichl's text].

(10.425) can be inverted to give

$$\frac{\rho_s^0}{\rho_n^0} = \frac{\tilde{c}_p c_2^2}{T^0 (s^0)^2} \quad \rightarrow \quad \frac{\rho_s^0}{\rho_n^0} + 1 = \frac{\rho^0}{\rho_n^0} = \frac{T^0 (s^0)^2 + \tilde{c}_p c_2^2}{T^0 (s^0)^2}$$

i.e.,

$$\frac{\rho_n^0}{\rho^0} = \frac{T^0 (s^0)^2}{T^0 (s^0)^2 + \tilde{c}_p c_2^2} \quad (10.426)$$

which means a measurement of the second sound speed c_2 can give us the mass concentrations of the normal & super fluids, provided an estimate of s^0 is available.

When He II is passed through a porous materials that allows only the flow of the superfluid, another density wave, called the **fourth sound**, is observed [see Problem S10.8].

Code

$$\mathbb{S} = \begin{pmatrix} \mathbf{z} & \boldsymbol{\theta} & \mathbf{i} \mathbf{k} \rho n & \mathbf{i} \mathbf{k} \rho s \\ \frac{\mathbf{i} \mathbf{k}}{\rho \kappa T} & \mathbf{i} \mathbf{k} P T & \mathbf{z} \rho n & \mathbf{z} \rho s \\ \mathbf{z} \left(s - \frac{1}{\rho} P T \right) & \frac{\mathbf{z} \rho c_p}{T} & \mathbf{i} \mathbf{k} \rho s & \boldsymbol{\theta} \\ \frac{\mathbf{i} \mathbf{k}}{\rho^2 \kappa T} & -\mathbf{i} \mathbf{k} \left(s - \frac{1}{\rho} P T \right) & \boldsymbol{\theta} & \mathbf{z} \end{pmatrix};$$

`(Det[S] /. PT -> 0) // Collect[#, z] & // Factor`

$$\frac{(k^2 + z^2 \kappa T \rho) (c_p z^2 \rho n + k^2 s^2 T \rho s)}{T \kappa T}$$

`sol = Solve[(Det[S] /. PT -> 0) == 0, z] // Flatten`

$$\left\{ z \rightarrow -\frac{\mathbf{i} \mathbf{k}}{\sqrt{\kappa T} \sqrt{\rho}}, z \rightarrow \frac{\mathbf{i} \mathbf{k}}{\sqrt{\kappa T} \sqrt{\rho}}, z \rightarrow -\frac{\mathbf{i} \mathbf{k} s \sqrt{T} \sqrt{\rho s}}{\sqrt{c_p} \sqrt{\rho n}}, z \rightarrow \frac{\mathbf{i} \mathbf{k} s \sqrt{T} \sqrt{\rho s}}{\sqrt{c_p} \sqrt{\rho n}} \right\}$$

`ψ = {ρz, Tz, vnz, vsz}; zero = {0, 0, 0, 0};`

`s0[i_] := S /. {PT -> 0, sol[i]};`

Solve[S0[1].ψ == zero, ψ]

Solve: Equations may not give solutions for all "solve" variables.

$$\left\{ \left\{ \text{Tz} \rightarrow -\frac{\mathbf{s} \cdot \mathbf{T} (\rho - \rho \mathbf{n} - \rho \mathbf{s}) \cdot \rho \mathbf{z}}{\rho (-c \rho \rho \mathbf{n} + \mathbf{s}^2 \cdot \mathbf{T} \cdot \kappa \mathbf{T} \cdot \rho \rho \mathbf{s})}, \right. \right. \\ \left. \left. \text{vnz} \rightarrow -\frac{(c \rho \rho - c \rho \rho \mathbf{s} - \mathbf{s}^2 \cdot \mathbf{T} \cdot \kappa \mathbf{T} \cdot \rho \rho \mathbf{s}) \cdot \rho \mathbf{z}}{\sqrt{\kappa \mathbf{T}} \cdot \rho^{3/2} (-c \rho \rho \mathbf{n} + \mathbf{s}^2 \cdot \mathbf{T} \cdot \kappa \mathbf{T} \cdot \rho \rho \mathbf{s})}, \text{vsz} \rightarrow -\frac{(-\mathbf{s}^2 \cdot \mathbf{T} \cdot \kappa \mathbf{T} \cdot \rho^2 + c \rho \rho \mathbf{n} + \mathbf{s}^2 \cdot \mathbf{T} \cdot \kappa \mathbf{T} \cdot \rho \rho \mathbf{n}) \cdot \rho \mathbf{z}}{\sqrt{\kappa \mathbf{T}} \cdot \rho^{3/2} (-c \rho \rho \mathbf{n} + \mathbf{s}^2 \cdot \mathbf{T} \cdot \kappa \mathbf{T} \cdot \rho \rho \mathbf{s})} \right\} \right\}$$

Solve[S0[4].ψ == zero, ψ]

Solve: Equations may not give solutions for all "solve" variables.

$$\left\{ \left\{ \rho \mathbf{z} \rightarrow \mathbf{0}, \text{Tz} \rightarrow -\frac{\sqrt{\mathbf{T}} \cdot \text{vnz} \cdot \sqrt{\rho \mathbf{n}}}{\sqrt{c \rho} \cdot \sqrt{\rho \mathbf{s}}}, \text{vsz} \rightarrow -\frac{\text{vnz} \cdot \rho \mathbf{n}}{\rho \mathbf{s}} \right\} \right\}$$